

# Accelerated Crevice Corrosion of Duplex Stainless Steels in Wet Limestone FGD Environments

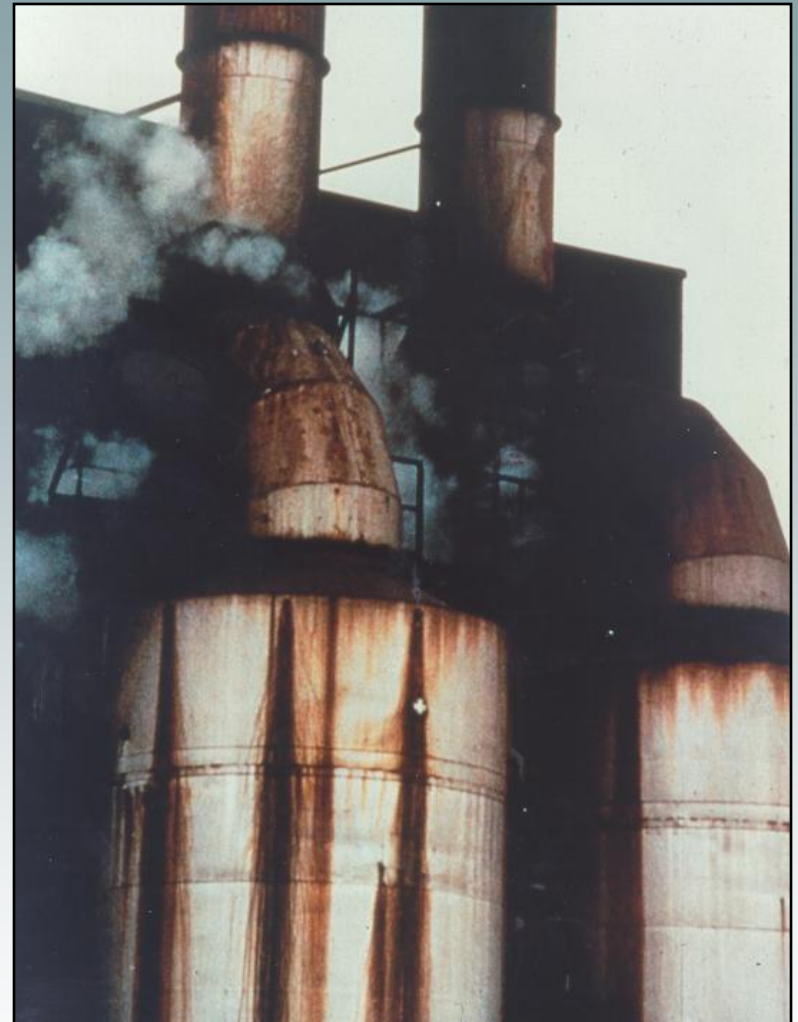
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# Outline

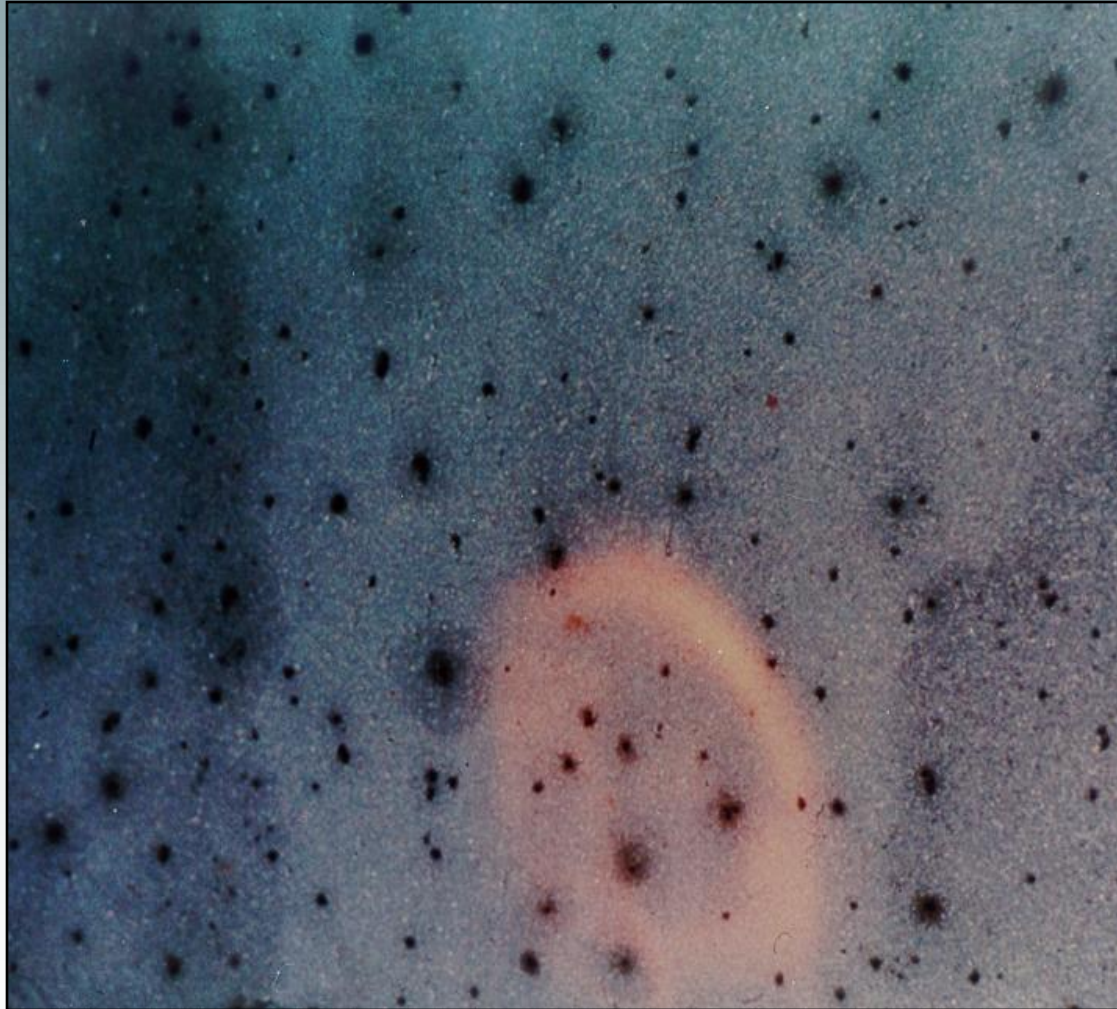
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- General comments on alloy crevice corrosion and conditions in FGD systems
- Recent observations of crevice corrosion in absorber vessels
- Results from on-site panel exposures
- Laboratory simulations
- Weld metal behavior



**Premature Failure of Absorber Vessels due to Corrosion**

# Pitting Corrosion



**Isolated pits widespread across surface**



# Crevice Corrosion

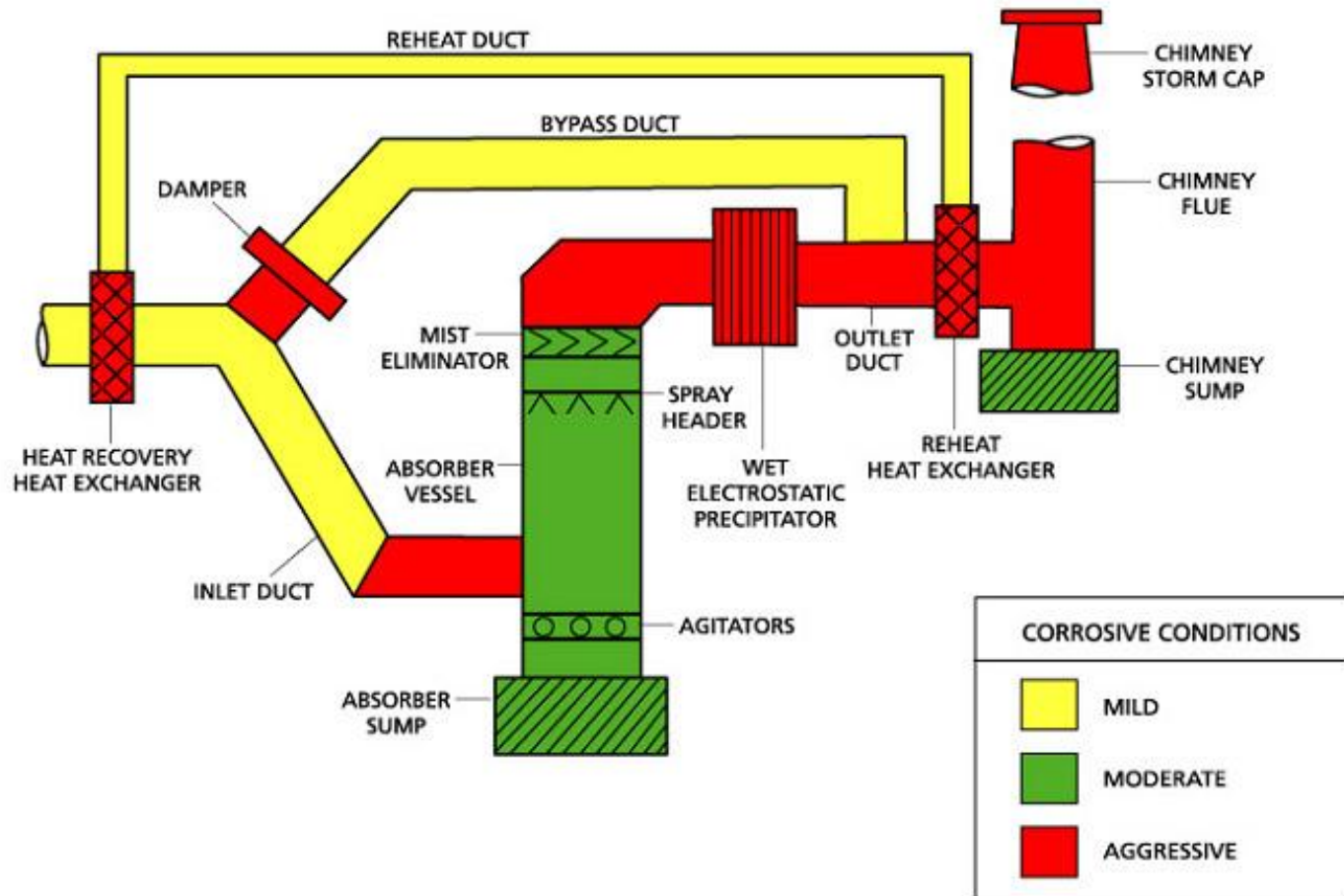


**Corrosion under ash deposit**

# Conditions in FGD Systems

- Sulfuric / sulfurous acids - pH 5.5 to <1
- Temperature - 125°F to boiling
- Halides - chlorides & fluorides
- Wet / dry (boiling) interfaces
- Crevice formers - flyash, lime, gypsum
- Salts - oxidizing and reducing
- Traces of hydrochloric & nitric acids
- **Solution may be much more corrosive under deposits**

## CORROSIVE CONDITIONS IN THE WET LIMESTONE FGD SYSTEM



**Generic diagram for illustration, individual plants vary in detail**

# Recent Absorber Vessel Construction in the USA

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- Shortage of Ni and Mo caused spike in alloy prices
- Ni-Cr-Mo alloys became too expensive
- Duplex stainless steels became an affordable alloy option
- In USA 85 FGD absorber vessels fabricated from 2205 duplex steel plate
- Severe corrosion and in some cases perforation experienced
- Following is an investigation Special Metals made at two mid-western plants

# Field Observations

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- **Two wet limestone FGD absorber vessels constructed of duplex steel plate were severely corroded after 7 months of operation.**
- **Severe attack was found adjacent to welds as well as remote from them. Crevice corrosion was believed to be the mode of attack.**
- **One scrubber was shut down for repair. The vessel was inspected and test samples were installed.**





**Crevice corrosion under the seal of 2205 duplex steel (S31803) entry cover of a wet limestone FGD absorber vessel after less than one year of operation**

**HAZ  
Attack**

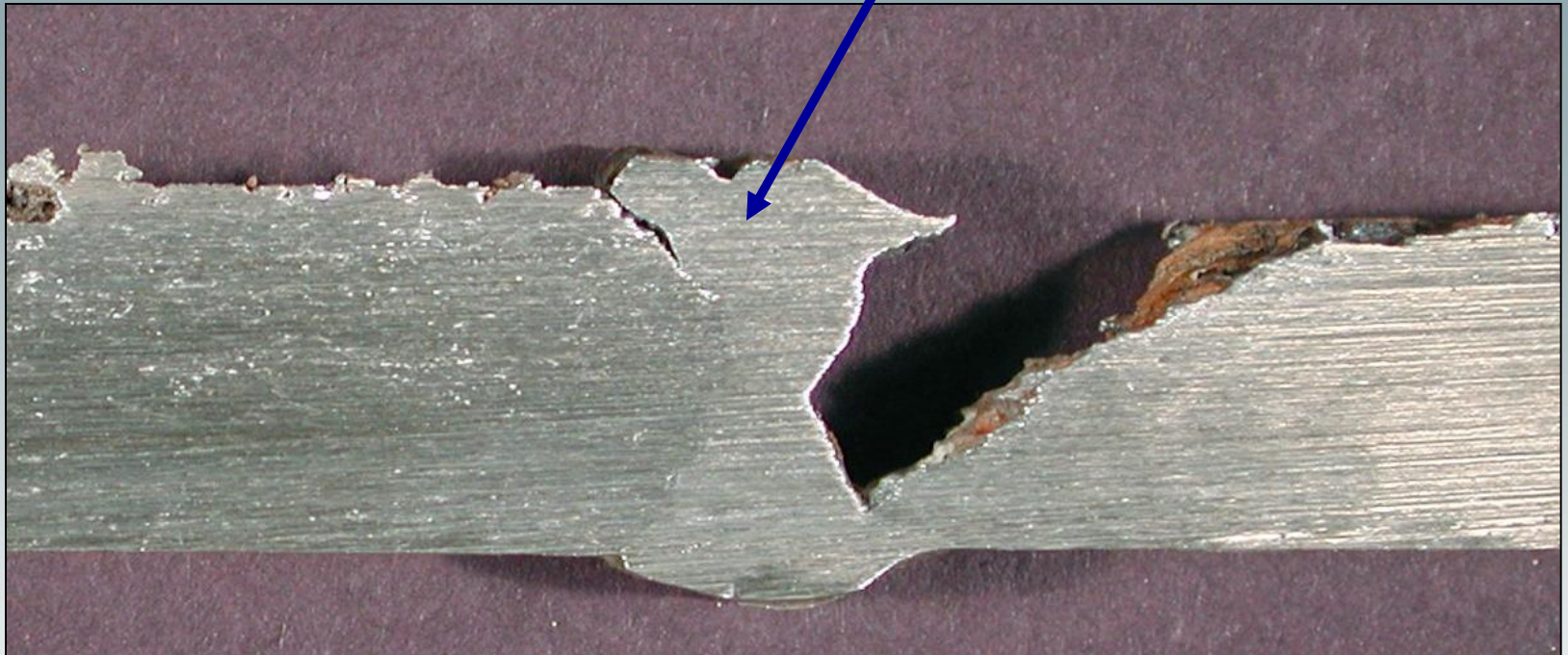


**Widespread  
crevice  
corrosion  
under deposits**



**Crevice corrosion of duplex steel  
absorber wall adjacent to alloy 625 weld**

**Alloy 625 weld nugget**



**Corroded duplex stainless steel absorber wall joined with NiCrMo 625 welding product. The weld nugget was not attacked but the base metal was nearly penetrated at the HAZ.**





**Corrosion of duplex steel absorber vessel. The nickel alloy 625 weld was not attacked.**





**Attack of 2205 duplex steel absorber. Bottom plate is original construction. Upper plate is repair. Weld is alloy 625.**



**Crevice corrosion of a section of the duplex steel absorber wall that appears to be weld-related, perhaps due to mineral deposit build-up by “proud” welds. The alloy 625 weld metal was not attacked.**





**Crevice corrosion of duplex steel absorber vessel wall  
located well away from weldment**

# Field Testing

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One foot square test specimens of were welded to the absorber wall

Materials tested were:

- Nickel Base alloys: N10276, N06686
- Super-austenitic stainless steels: N08926, S31277
- Duplex steel (as control sample) - S31803

Prior to installation, a weld was deposited on each sample to evaluate the effect of welding





**Duplex Steel (S31803)**

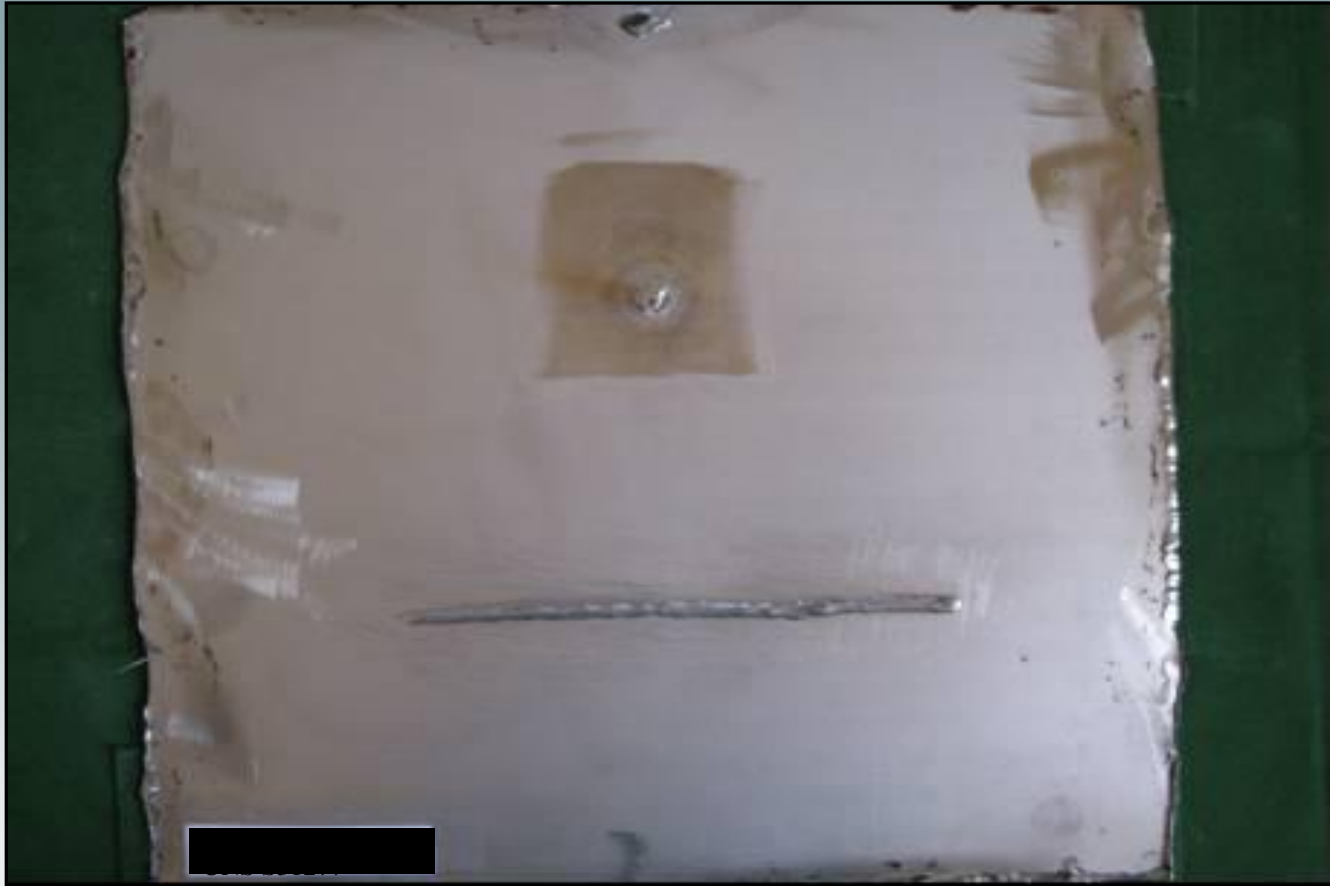


**Super-Austenitic Steel (S31277)**

**Test panels exposed 7 months on the absorber vessel wall.  
Mineral buildup is believed to have induced crevice condition.  
Note adherent black film.**



**Duplex steel test panel after cleaning. Attack is evident, especially near the weld.**



**Super-austenitic steel (S31277) test panel after cleaning. No attack was found.**



**NiCrMo alloy N10276**



**NiCrMo alloy N06686**

**Ni-base alloy test panels after cleaning. No attack was found.**



# Laboratory Testing Nickel Alloys & Stainless Steels in a Simulated FGD Solution

Objective was to reproduce conditions under a deposit




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Alloy	2205	2507	316L	25-6MO	27-7MO	C-276
Rate (mpy)	1864	1999	37	2	5	5




- **60% H<sub>2</sub>SO<sub>4</sub> + 0.5% HCl + 0.2% HF + 0.1% HNO<sub>3</sub>**
- **70 C (158 F)**

# Appearance of Coupons After Test

Test Environment: 60% H<sub>2</sub>SO<sub>4</sub> + 0.5% HCl + 0.2% HF + 0.1% Nitric at 70°C for one week.

Alloy		
UNS S31603	UNS S31803	UNS S32750
Corrosion Rate		
37 MPY	1864 MPY	1999 MPY
		

Alloy		
UNS N08926	UNS S31277	UNS N10276
Corrosion Rate		
2 MPY	5 MPY	5 MPY
		

# **Welding Product Selection**

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**Use overmatching composition welding products to offset iron dilution & elemental segregation in NiCrMo & FeNiCrMo corrosion resistant alloys and stainless steels**

# Preferential attack of NiCrMo C-276 filler metal welds in FGD outlet duct

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**Alloy C-276 base plate**



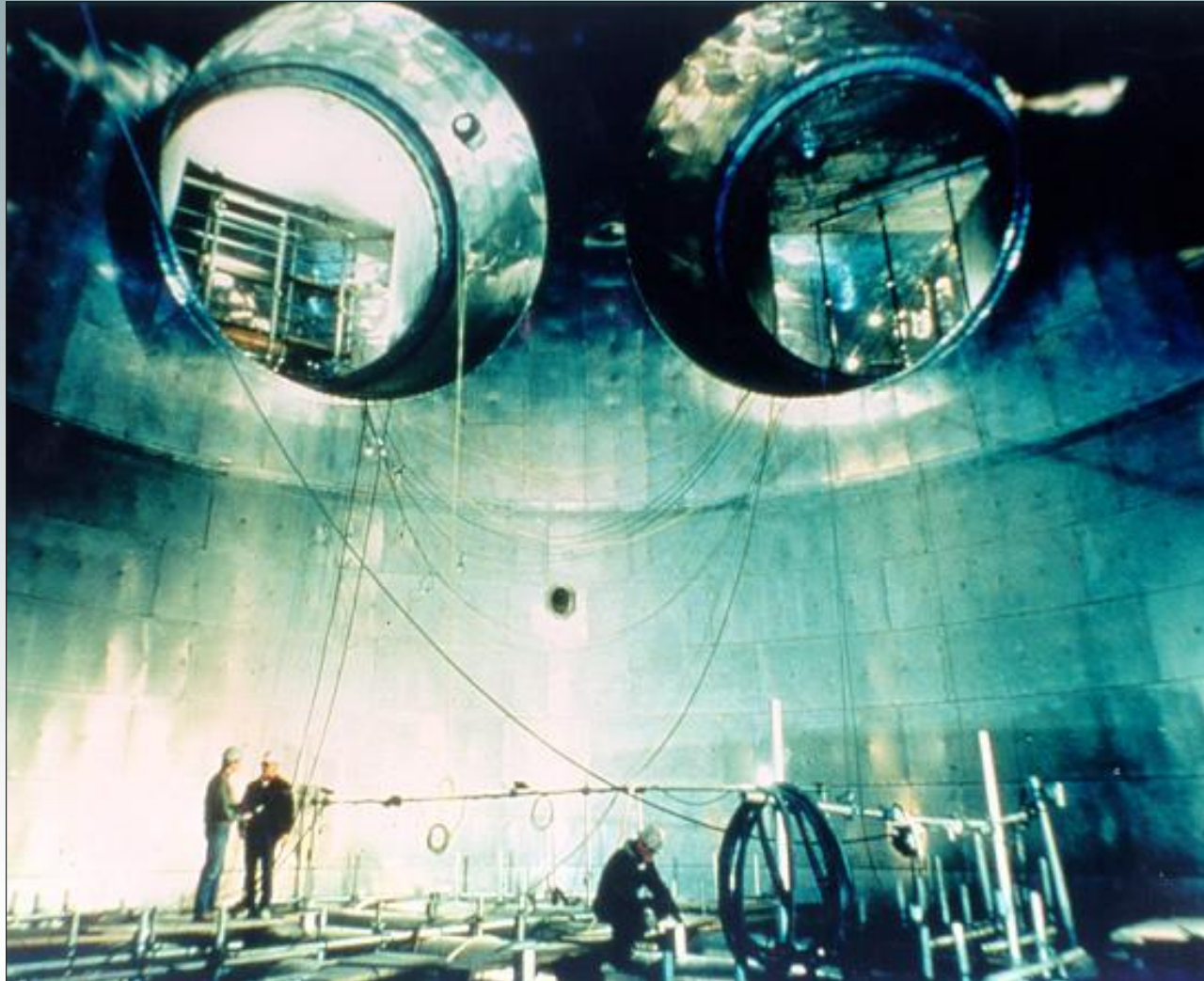
# Overmatched NiCrMo 686 filler metal welds after six months FGD service



**Alloy C-276 Base plate**

# Nickel-Alloy, Wallpaper-Lined FGD Absorber Vessel

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# Nickel-Alloy Lined FGD Duct

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# Super-Austenitic Steel Chimney Flue at APS-Cholla Station

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**27-7MO (S31277) plate joined with 686 (N06686) welding product**



# In Summary

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- **Corrosive conditions under tightly adhering deposits may lead to unpredicted crevice corrosion attack**
- **Super-austenitic stainless steels offer an economical alternative to high nickel alloys in some sections of the wet FGD scrubber**
- **Wallpaper cladding offers a proven repair strategy**
- **Overmatching composition welding products are required to produce fully resistant welds.**

# Clean Air & Clear Skies

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